DESIGN AND MANUFACTURING OF A LEAF SPRING USING COMPOSITE MATERIALS

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Abstract— A leaf spring is a simple form of spring, commonly used for the suspension in wheeled vehicles. Leaf Springs are long and narrow plates attached to the frame of a trailer that rest above or below the trailer's axle. There are mono leaf springs, or single-leaf springs, that consist of simply one plate of spring steel. These are usually thick in the middle and taper out toward the end, and they don't typically offer too much strength and suspension for towed vehicles. Drivers looking to tow heavier loads typically use multi leaf springs, which consist of several leaf springs of varying length stacked on top of each other. The shorter the leaf spring, the closer to the bottom it will be, giving it the same semielliptical shape a single leaf spring gets from being thicker in the middle.

Keywords—Leaf Spring, Composite Materials

1. INTRODUCTION

The aim of the project is to design and model a leaf spring according to the loads applied for the material carbon epoxy. While designing leaf spring we are going to consider following five cases.

- Case I Thickness is the variable
- Case 2- Camber is the variable
- Case 3 Span is variable

Case 4 – Number of leaves is the variable

- We are also considering these cases also
 - Modeling of Road Irregularity
 - Variation of Exciting frequency with vehicle speed

Presently Used Material For Leaf Spring Are Forged Steel. In This Project We Are Going To Design Leaf Spring For The Material Composite Material Carbon Epoxy By Varying Reinforcement Angle And Layers. We Are Going To Check The Strength Variations While Changing Reinforcement Angle And Layers. For Validating This Design We Are Conducting Fea Structural Analysis Is Done On The Leaf Spring By Using Two Different Material Carbon Epoxy

2. COMPOSITE MATERIALS

These are materials with two or more compositions mainly now a days composite materials are became more popular and friendly because of its various advantages in this I have worked on two different composite materials and compared with conventional materials.

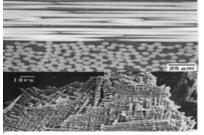


FIGURE 1 Cross section of a graphite fiber-reinforced epoxy polymer

Physical Properties	Metric
Density	2.46 g/cc
Mechanical Properties	Metric
Tensile Strength, Ultimate	4890 MPa
Elongation at Break	5.70 %
Modulus of Elasticity	86.9 GPa
Poissons Ratio	0.230
Shear Modulus	35.0 GPa

3. DESIGN CALCUCULATION OF LEAF SPRING

When n=10, Rear suspension Number of leaf springs = 4 Overall length of the spring = 2L1 = 137.2cm = 1372mmWidth of leaves = 76.2 = 80mmNumber of full length leaves = 2 = nfNumber of graduated leaves = 8 = NgNumber of springs = 10 (Ng+Nf)Center load = 2W = 115 tones = 11500kg 2W = 11500 9.8 = 112700N2W = 112700/4 = 28175N

$$2W = \frac{\text{total load}}{\text{no of springs}} = 28175N$$

$$W = 14087.5N$$

3.3.1 Bending Stress

Bending stress, $\sigma = \frac{6 W L_1}{nbt^2}$

 $=\frac{6\times14101.875\times686}{10\times80\times16^2}$

 $= 283.4146 \text{ N/mm}^2$

Bending stress, $\sigma = 283.4146 \text{ N/mm}^2$

Spring is simply supported beam



Width length = 2L

Central load =2W

Deflection for both full length and graduated leaves

$$y = \delta = \frac{6WL^3}{n\epsilon bt^3} = \frac{6\times 14101.875 \times 686^3}{10\times 80 \times 86900 \times 16^3} = 95.923 \text{ mm}$$

Radius of curvature

 $R = \frac{{L_1}^2 + y^2}{2y} = \frac{686^2 + 95.923^2}{2 \times 95.923} = 2500.91 \text{ mm}$

 \therefore Radius of curvature = 2500.91 mm

3.3.2 Length of leaf springs

 $2L_1 = overall \ length \ of \ spring$ Ineffective length 1 = width of band/distance between centers of u-tubes

Effective lengths $2L = 2L_1 - \frac{2}{3}l$ (when u bolts are used) $L_1 = 1372$ mm l= 300 (assume) $2L = 1372 - \frac{2}{3} \times 300 = 1172$ mm

It may be noted that when there is only one full length leaf (master leaf only) then the no of leaves to be cut will be n and when there are two full length leaves (including one master leaf) then the no of leaves to be cut will be (n-1) if a leaf spring has two full length leaves then the length of leaves is obtained as follows

Length of smallest leaf = $\frac{effective length}{1}$ + ineffective length n= 12 $=\frac{1172}{9} + 300$ = 430.22 mm Length of next leaf = $\frac{effective \ length}{2} \times 2 + ineffective \ length$ $=\frac{1172}{9} \times 2 + 300$ =560.44 mm Length of 3^{rd} leaf = $\frac{1172}{2} \times 3 + 300 = 690.66$ mm Length of 4^{rd} leaf $=\frac{1172}{2} \times 4 + 300 = 820.88$ mm Length of 5^{rd} leaf = $\frac{1172}{2} \times 5 + 300 = 951.1$ mm Length of 6^{rd} leaf $=\frac{1172}{9} \times 6 + 300 = 1081.32$ mm Length of 7^{rd} leaf = $\frac{1172}{2} \times 7 + 300 = 1211.54$ mm Length of 8^{rd} leaf = $\frac{9}{1172} \times 8 + 300 = 1341.76$ mm Length of 9^{rd} leaf $=\frac{1172}{9} \times 9 + 300 = 1471.98$ mm The nth leaf will be the master leaf and it is of full length since the master leaf has eyes on both sides therefore Length of master leaf = $2L_1 + \pi(d + t) \times 2$ d = Inside diameter of eye t = thickness of master leaf d =22 mm $t=1372+\pi (22+22)\times 2$ t = 1648.46 mm**Research script | IJRME**

The approximate relation between the radius of curvature

 $R = \frac{L_1^2}{2\nu}$ (R) and camber (Y) of spring is given by $L_1 = half span of spring$ Y = δ (the maximum deflection of spring is equal to camber(y) of spring)

$$L_1 = \frac{1372}{2} = 686$$
mm ; $\delta =$

95.923mm

$$R = \frac{L_1^2 + y^2}{2y} = \frac{686^2 + 95.923^2}{2 \times 95.923} = 2500.91 \text{ mm}, \delta = 95.923 \text{ mm}$$

3.3.3 Radius values

1 = 2644.91 mm2 = 2628.91 mm 3 = 2612.91 mm4 = 2596.91 mm 5 = 2580.91 mm 6 = 2564.91 mm 7 = 2548.91 mm 8 = 2532.91 mm 9 = 2516.91 mm3.3.4 Modelling and analysis of the leaf spring

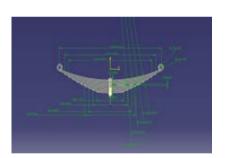


FIGURE 2 3D MODEL OF LEAF SPRING CASE 1:- MATERIAL - MILD STEEL Save CATIA Model as .iges format $\rightarrow \rightarrow$ Ansys \rightarrow Workbench \rightarrow Select analysis system \rightarrow

static structural \rightarrow double click \rightarrow Select geometry \rightarrow right click \rightarrow import geometry \rightarrow

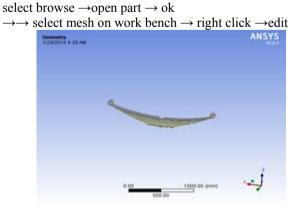


Figure3 Imported model into ANSYS work bench

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 $mesh \rightarrow$

Double click on geometry \rightarrow select geometries \rightarrow edit material \rightarrow

4. MATERIAL PROPERTIES OF STEEL

Density : 0.00000785kg/mm³ Young's modulus : 20000Mpa passions ratio : 0.3Select mesh on left side part tree \rightarrow right click \rightarrow generate

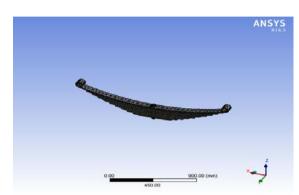


Figure4: Meshing of the component

Select static structural right click \rightarrow insert \rightarrow select force - 14088 N

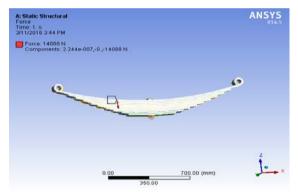
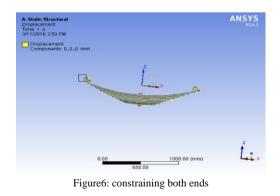


Figure5: Applying force on the leaf spring

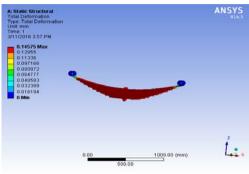
Select displacement \rightarrow select required area \rightarrow click on apply \rightarrow put X,Y,Z component zero \rightarrow



Solution right click \rightarrow insert \rightarrow deformation \rightarrow total \rightarrow Solution right click \rightarrow insert \rightarrow strain \rightarrow equivant (vonmises) \rightarrow

Solution right click \rightarrow insert \rightarrow stress \rightarrow equivant (vonmises) \rightarrow

Right click on deformation \rightarrow evaluate all result





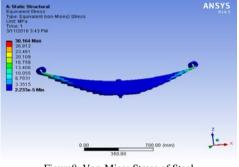
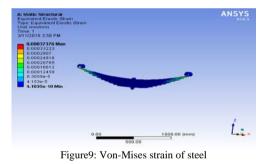


Figure8: Von-Mises Stress of Steel



CASE 2:- MATERIAL - CARBON EPOXY MATERIAL PROPERTIES OF CARBON EPOXY Density : 1.60 g/cc

Density Young's modulus	: 1.60 g/cc : 70.0GPa	
Possions ratio	: 0.3	
A: State Structured Total Centermation Type: Total Deformation Type: Total Deformation Type: 31112016 4 21 PM 0.0641033 0.0641033 0.0641033 0.034651000000000000000000000000000000000000		ANSYS
	0.00 600.00 (mm)	لمنه

Figure10: Total Deformation of Carbon Epoxy

Select solution right click \rightarrow solve \rightarrow

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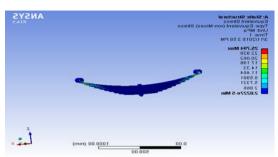


Figure11: Von-Mises Stress of Carbon Epoxy

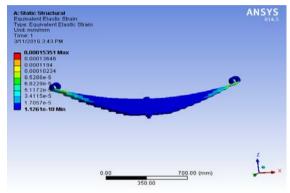


Figure12: Von-Mises Strain of Carbon Epoxy

CASE 3:- MATERIAL - S2 GLASS MATERIAL PROPERTIES OF S2 glass

Density 2.46 g/cc

86.9GPa Young's modulus : Possions ratio

0.28

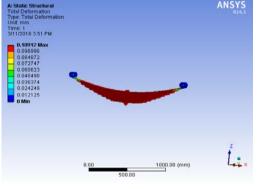


Figure 13: Total deformation of S2 Glass

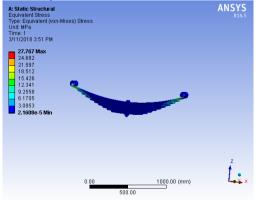


Figure 14: von-mises Stress of S2 Glass

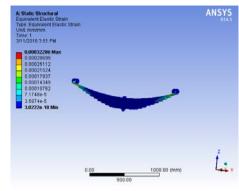
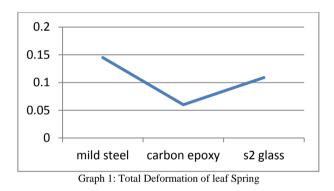


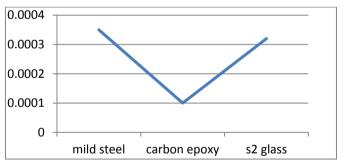
Figure 15: Von-Mises Strain of S2 Glass

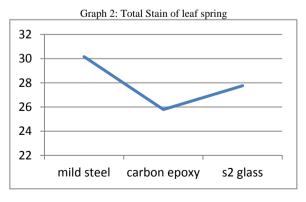
5. RESULTS AND DISCUSSIONS

TABLE 2 : RESULTS OF THE LEAF SPRING

	Mild steel	Carbon epoxy	S2 glass
Deformation (mm)	0.145	0.0693	0.10912
STRESS (N/mm ²)	30.164	25.79	27.76
STRAIN	0.00035	0.00015	0.00032
Graphs			







Graph3: Total stress of leaf spring



6. CONCLUSION

The data is collected from net for the specifications of the model. The leaf spring is designed for the load of 14087.5N. Theoretical calculations have been calculated for leaf spring dimensions at different cases like varying thickness, camber, span and no. of leaves by mathematical approach. In this thesis, analysis have been done by taking materials steel, carbon Epoxy and s2 glass Structural analysis are conducted on total assembly of leaf spring. The stresses in the composite leaf spring of design are much lower than that of the allowable stress. The strength to weight ratio is higher for composite leaf spring than conventional steel spring with similar design.

The major disadvantages of composite leaf spring are the matrix material has low chipping resistance when it is subjected to poor road environments which may break some fibers in the lower portion of the spring. This may result in a loss of capability to share flexural stiffness. But this depends on the condition of the road. In normal road condition, this type of problem will not be there. Composite leaf springs made of polymer matrix composites have high strength retention on ageing at severe environments.

The steel leaf spring width is kept constant and variation of natural frequency with leaf thickness, span, camber and numbers of leaves are studied. It is observed from the present work that the natural frequency increases with increase of camber and almost constant with number of leaves, but natural frequency decreases with increase of span. The natural frequencies of various parametric combinations are compared with the excitation frequency for different road irregularities. The values of natural frequencies and excitation frequencies are the same for both.

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